

A fully differential architecture of folded cascode OTA is selected as it suppresses the even harmonics which are dominant in single ended OTA structure and also because of its higher common mode rejection ratio (CMRR) and improved dynamic range [9]-[11]. The transistors are operated in sub-threshold region to reduce the power and make it suitable for low power applications. The biasing currents used are 100nA with a supply voltage of +/- 1V.

B. Common Mode Feedback Circuit (CMFB)

Fig. 2. shows the block diagram of the common mode feedback circuit (CMFB) required for the fully differential OTA structure. CMFB circuit performs three operations: it senses the common mode outputs of the fully differential OTA then compares the result with a reference voltage, normally the reference voltage (V_{ref}) is equal to half of the supply voltage, for +/- supply voltage the reference voltage should be zero; and then returns the error to the amplifiers bias network (VCMC) using negative feedback to set the common mode (CM) output value [12]. The schematic of CMFB is shown in Fig. 3.

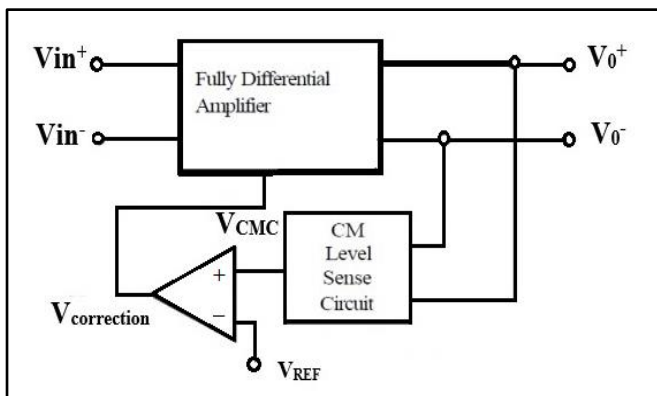


Fig. 2. Block diagram of Common mode feedback circuit

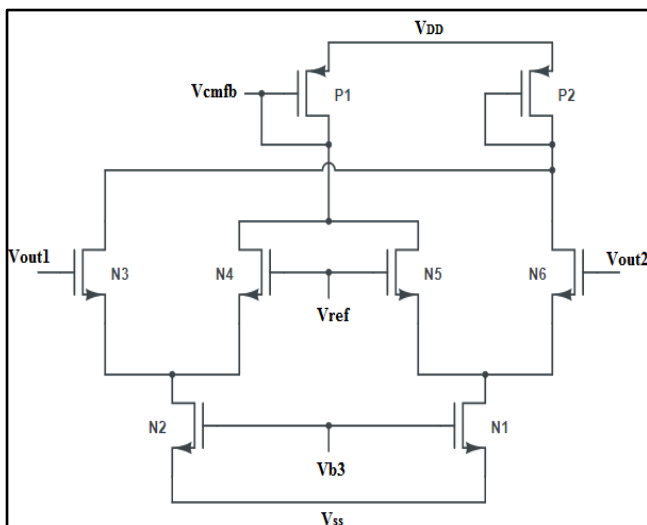


Fig. 3. Common mode feedback circuit

III. SIMULATION RESULTS

The simulations for the folded cascode OTA structure is carried out in CADENCE environment using 150nm CMOS technology. Fig.4. shows the simulated results for the gain, phase and unity gain bandwidth (UGBW). Fig. 5. shows CMRR graph and input referred noise plot is shown in Fig. 6.

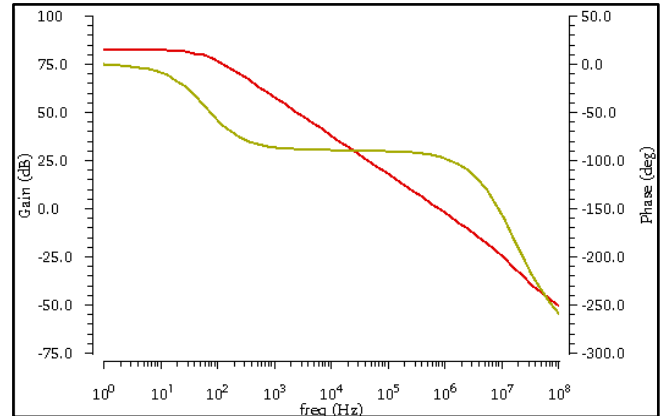


Fig. 4. Gain and phase of folded cascode OTA

The DC gain is 82 dB with phase margin of 84 degrees and UGBW of 768 KHz. The power dissipation of the circuit is 834.2nW which is suitable for low power applications. The OTA parameters and the aspect ratios of the transistors are tabulated in Table I and Table II respectively.

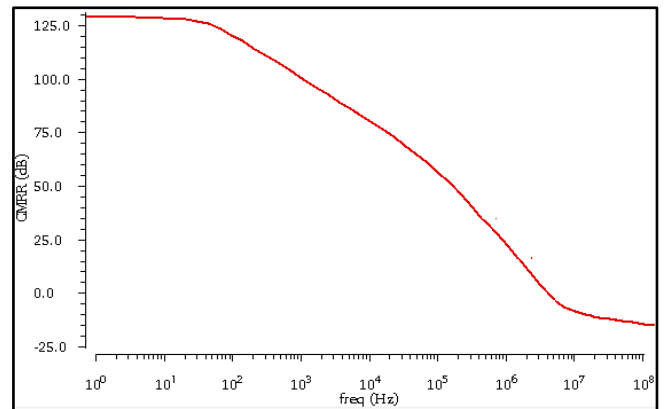


Fig. 5. CMRR of folded cascode OTA

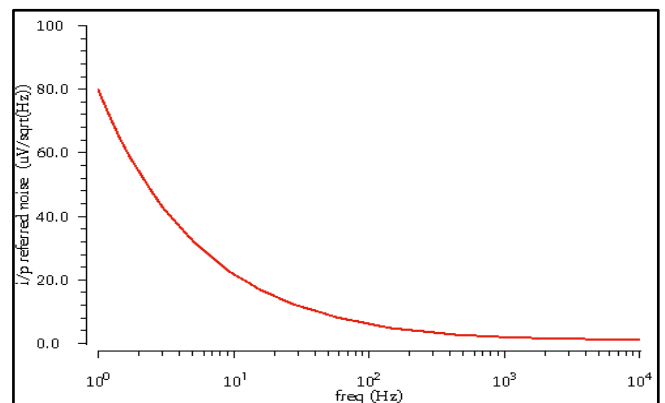


Fig. 6. Input referred noise plot in uV/sqrt(Hz)

TABLE I. DIFFERENT OTA PARAMETERS

Parameters	Values
Technology	150nm
Supply Voltage	+/- 1V
Gain	82 dB
Phase Margin	84 ⁰
UGBW	768 KHz
CMRR	128 dB
Input ref. Noise	428.2uVrms
Power dissipation	834.2nW

TABLE II. ASPECT RATIOS FOR OTA TRANSISTOS

Transistors	W/L ratios
M1, M1'	10u/500n
M2,M3	4u/500n
M4,M5	8u/500n
M6,M7	4u/500n
M8,M9,M10,M11	4u/500n

IV. CONCLUSION

This paper describes the fully differential folded cascode OTA structures with common mode feedback circuit. This OTA is operated in sub-threshold region to reduce the power consumption. The input differential pair utilizes PMOS transistors to reduce the flicker noise which is less in PMOS compare to NMOS. The fully differential OTA structure requires a common mode feedback circuit to stabilize the common mode output because it is quite sensitive to the device properties and mismatches [13]. Different parameters of the OTA are simulated using 150nm CMOS technology in CADENCE environment. The power consumption of the circuit is in nano watt which is quite low and is suitable for low power applications.

REFERENCES

- [1] Wen-Yaw Chung, Chung-Cheng Chuang, Ying-Hui Zheng and Ying-Hsiang Wang, 'A new low power low voltage OTA for ECG Readout Circuit Design', Journal of Medical and BIOLOGICAL Engineering, Vol. 26, No. 4, pp. 195-202, 2006.
- [2] Aimad El Mourabit, Guo-Neng Lu and Patrick Pillet, 'Wide-Linear-Range, Subthreshold OTA for Low-power, Low-voltage and Low-frequency Applications', IEEE Transactions on Circuits and Systems-I, Vol. 52, NO.8, pp. 1481-1488, August 2005.
- [3] Meysam Akbari, Masoud Nazari, Leila Sharifi and Omid Hashemipour, 'Improving power efficiency of two stage operational amplifier for biomedical applications', Analog Integrated Circuits and Signal Processing, vol. 84, p. 173-18, 2015.
- [4] Marie Joyce Cabebe, Charlee Dave Gallego, John Richard Hizon and Louis Alarcon, 'Design Tradeoffs in a 0.5V 65nm CMOS Folded Cascode OTA', IEEE TENCON, 2013.
- [5] Okkes Gokalp Sokmen, Hamdi Ercan, Sezai Alper Tekin and Mustafa Alci, 'A Novel Low Voltage Low Power OTA Based on Level Shifter Current Mirror', ELEKTRONIKA IR ELEKTROTEHNIKA, ISSN 1392-1215, VOL. 21, NO. 2, 2015
- [6] Evandro Daniel C. Cotrim and Luis H. de Carvalho Ferreira, 'An ultra-low-power CMOS symmetrical OTA for low frequency Gm-C applications', Analog Integrated Circuits and Signal Processing, Vol. 71, pp. 275-282, 2012.
- [7] Alfio Dario Grasso, Gaetano Palumbo and Salvatore Pennisi, 'High-Performance Four Stage CMOS OTA Suitable for Large Capacitive Loads', IEEE Transactions on circuits and systems-I, Vol. 62, No. 10, pp. 2476-2484, October 2015.
- [8] Jianglong Chen, Edgar S. Sinencio and Jose Silva, 'Frequency Dependence Harmonic Distortion of a Linearized Cross-Coupled CMOS OTA and its Applications to OTA-C Filter', IEEE Transactions on circuits and systems-I, Vol. 53, No. 3, pp. 499-510, March 2006.
- [9] S-Yuh Lee and C-Jen Cheng, 'Systematic design and modeling of OTA-C Filter for portable ECG detection', IEEE Transaction on Circuits and Systems, Vol. 3, No.1, pp. 53-63, February 2009.

- [10] Ahmed Nader Mohilden, E. Sached-Senencio and Jose Silva –Martinez, 'A fully balanced pseudo-differential OTA with common-mode feedforward and inherent common-mode feedback detector', IEEE Journal of solid state circuits, Vol. 38, NO. 4, pp. 663-668, April 2003.
- [11] Wang Chunhua, Leng Yang, Zhang Qiuqing, Fei Yu, 'Systematic Design of Fully Balanced Differential CurrentMode Multiple-Loop Feedback Filters Using CFBCII', Radioengineering, Vol. 19, NO.1, pp. 185-193, April 2010.
- [12] Apirak Suadet and Varakon Kasemsuwan, 'A Current-Mode Common-Mode Feedback Circuit (CMFB) with rail to rail operation', Frequenz, Vol. 65, pp. 4-54, 2011.
- [13] Behzad Razavi, 'Design of Analog Integrated Circuits', McGRAW-HILL International Edition, Electrical Engineering Series, 2001.